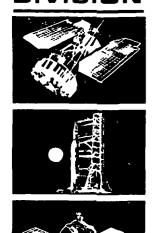
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SPACE















CASE FILE COPY

FINAL REPORT

REDUCTION OF
TRUNCATION ERRORS
IN
MODAL ANALYSIS

ADDENDUM

DAMUS USERS MANUAL

PREPARED FOR:

NATIONAL AERONAUTICS
AND
SPACE ADMINISTRATION
GEORGE C. MARSHALL SPACE FLIGHT CENTER
UNDER:
CONTRACT NAS 8-28167

GENERAL ELECTRIC

GE Document No. 73SD4251 June 29, 1973

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Prepared for

George C. Marshall Space Flight Center

Prepared Under:

Contract NAS 8-28167

NASA-MSFC Technical Monitor: Dr. J.R. Admire

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FOREWORD

The program reported herein was performed by the General Electric-Space Division, Valley Forge, Pa., for the George C. Marshall Space Flight Center, Marshall Space Flight Center, Alabama, under Contract NAS 8-28167. The performance period for the work was 2 December 1971 to 29 June 1973. The principal investigator was Edward J. Kuhar and the program manager was Clyde V. Stahle. The NASA Technical Monitor was Dr. John R. Admire who provided valuable guidance throughout the course of the program.

The results of the study are described in the main volume of this report and include the theoretical development of the dynamic transformation method, numerical results from the application of the method to several sample problems, and some comparisons with other available methods of analysis.

The separate addendum to this report provides the user instructions for the DAMUS computer program (Dynamic-transformation Adapted to Modal-synthesis Using Stiffness Coupling) which implements the method developed under this program.

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Nomenclature

[m]	=	mass matrix for substructure in	{x}	physical
		coordinates		

$$\left[\emptyset \right] = \underset{\text{coordinates}}{\text{matrix of substructure eigenvectors in }} \left\{ x \right\}$$

[
$$\gamma$$
] = matrix of eigenvectors for total structure in $\{q\}$ modal coordinates

[R] = transformation matrix defining the relationship of the reduced coordinates,
$$\{q^R\}$$
, to the kept coordinates $\{q^K\}$.

$$\{x\}$$
 = physical coordinates

$$\Omega$$
 = system circular frequency

$$\omega$$
 = substructure circular frequency

Subscripts

i = refers to the ith subset, term, or substructure

CPL = incremental stiffness from coupling spring

k = kept coordinates

r = reduced coordinates

Superscripts

k = kept coordinates

r = reduced coordinates

A = attachment coordinates

I = interior coordinates not attached to any other sub-

structure

= revised value

•• second time derivative

ij = particular submatrix partition

SECTION 1

INTRODUCTION

This document describes a Fortran IV computer program used to perform modal synthesis by stiffness coupling using the dynamic transformation method. The program has been named DAMUS (Dynamic-transformation Adapted to Modal-synthesis Using Stiffness-coupling). The program begins with the entry of a substructure's mass and stiffness matrix. The eigenproblem for the individual substructure is solved. Provisions are included for a maximum of 20 substructures (100 DOF max/substructure) which may be coupled by 100 stiffness matrix springs (100 DOF/spring). The substructures are then coupled together via coupling springs, and the dynamic transformation is used to reduce the size of the eigenproblem. After solving for the coupled system eigenvalues and vectors, the user may elect to backsubstitute selected modes. The total number of modes treated by the program is 300 consisting of 100 kept coordinates (maximum eigenvalue size) and 200 coordinates reduced by the dynamic transformation. For user flexibility, six major entry points have been included in DAMUS,

Input data for DAMUS is mainly accomplished by the READ and READIM FORMA subroutines. Output data to be saved is written on files generated by the WTAPDS and WTAPSS subroutines written specifically for DAMUS. Those files which contain data to be saved should be copied to tape after the execution of DAMUS. A total of 12 files have been defined for use by the program. Depending on user options, the number of files used at any one time will vary; and at no time will all twelve be used simultaneously.

SECTION 2

THEORETICAL DISCUSSION

2.1 BASIC THEORY FOR STIFFNESS COUPLING

The stiffness coupling method of modal synthesis assembles the complete structure in the same manner as the displacement method for structural analysis. The total structure may be represented by a number of substructures connected through flexible links. Each substructure is analyzed without the flexible links to determine the component vibration modes with free attachment coordinates. The flexible links are represented by a stiffness matrix relating the interface forces from one set of substructure attachment coordinates to another.

The method of substructuring for stiffness coupling may best be illustrated by considering a total structure consisting of only two substructures. The general undamped equation of motion for the ith substructure in terms of its generalized mass matrix, $[m_i]$, and generalized stiffness matrix, $[k_i]$, is given by

$$[m_i] \{ x_i \} + [k_i] \{ x_i \} = 0$$
 (1)

where the coordinates $\{\chi_i\}$ describe physical motions of the mass points. Each substructure has two sets of coordinates which will be referred to as attachment coordinates, $\{\chi_i^A\}$, and internal coordinates, $\{\chi_i^I\}$. The attachment coordinates are those degrees of freedom (DOF) which are connected to another substructure via a stiffness matrix or coupling spring. The internal

coordinates are those DOF which are not connected to any other substructure. It is important to note that for stiffness coupling the coordinates belonging to one particular substructure are not common to any other. If n; represents the size of the ith substructure and n the size of the total structure comprised of Λ substructures, then n will be given by

$$N = \sum_{i=1}^{\Lambda} n_i \tag{2}$$

Having defined two sets of coordinates for each substructure, Eq. (1) may be written in partitioned form as

$$\begin{bmatrix}
 m_i^{1} & m_i^{12} \\
 m_i^{2} & m_i^{22}
\end{bmatrix}
\begin{cases}
 \frac{\circ A}{\chi_i} \\
 \frac{\circ I}{\chi_i}
\end{cases}
+
\begin{bmatrix}
 k_i^{1} & k_i^{12} \\
 k_i^{21} & k_i^{22}
\end{bmatrix}
\begin{cases}
 \chi_i^{A} \\
 \chi_i^{I}
\end{cases}
= 0$$
(3)

Now consider the total structure to be described by a mass matrix, $[M_{\tau}]$, and a stiffness matrix, $[K_{\tau}]$, such that

$$[M_T] \{ \mathring{\chi}_T \} + [K_T] \{ \chi_T \} = 0$$

$$n \times n \quad n \times 1 \quad n \times n \quad n \times 1$$

$$(4)$$

where

$$\begin{bmatrix} M_T \end{bmatrix} = \begin{bmatrix} M_T^{1} & 0 \\ -\frac{1}{2} & -\frac{1}{2} \\ 0 & M_T^{22} \end{bmatrix} n_2$$

$$\begin{bmatrix} K_T \end{bmatrix} = \begin{bmatrix} K_T^{"} & K_T^{'2} \\ K_T^{21} & K_T^{22} \end{bmatrix} n_1$$

$$n_2$$
(5)

$$\left\{\chi_{T}\right\} = \left\{\frac{\chi_{1}}{\chi_{2}}\right\} \begin{array}{c} n_{1} \\ n_{2} \end{array}$$

If we describe the connecting structure between $\{\chi_i^A\}$ and $\{\chi_i^A\}$ by a mass matrix, $[m_{\Delta}]$, where

$$\begin{bmatrix} m_{\Delta} \end{bmatrix} = \begin{bmatrix} m_{\Delta_1}^{11} & 0 \\ -\frac{1}{1 - \frac{2z}{2z}} \\ 0 & m_{\Delta_2}^{A} \end{bmatrix} n_z^{A}
n_1^{A} n_2^{A}$$
(6)

and a stiffness matrix, $[k_{cpl}]$, relating the nodal forces, $\{F_i^A\}$, to $\{\chi_i^A\}$ by the equation

$$\begin{cases}
\frac{F_{i}^{A}}{F_{z}^{A}} = \begin{bmatrix} k_{cpL} & k_{cpL} \\ k_{cpL} & k_{cpL} \end{bmatrix} \begin{cases} \chi_{i}^{A} \\ \chi_{z}^{A} \end{cases} n_{i}^{A} \\ (n_{i}^{A} + n_{z}^{A}) \times I \qquad n_{i}^{A} \qquad n_{z}^{A} \end{cases}$$
(7)

Then $[M_T]$ and $[K_T]$ may be written in partitioned form using the submatrices defined by Eqs. (3), (6) and (7):

$$\begin{bmatrix} K_{T} \\ \end{bmatrix} = \begin{bmatrix} k_{1} + k_{CPL} & k_{1} & k_{CPL} & 0 \\ - & + & - & - & - \\ k_{2} & k_{1} & k_{2} & 0 & 0 \\ - & + & - & - & - & - \\ k_{1} & k_{2} & k_{2} & 0 & 0 \\ - & + & - & - & - & - \\ k_{1} & k_{2} & k_{2} & 0 & 0 \\ - & - & + & - & - & - \\ k_{1} & k_{2} & k_{2} & 0 & 0 \\ - & - & - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - & - \\ k_{1} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - & - \\ k_{1} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - \\ k_{1} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{1} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} & k_{2} \\ - & - & - \\ k_{2} & k_{2} &$$

By defining

$$\begin{bmatrix} M_{\Delta} \\ n \times n \end{bmatrix} = \begin{bmatrix} m_{\Delta_1} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & m_{\Delta_2} & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} n_1^A \\ n_1^T \\ n_2^A \\ n_2^T \\ n_2^T \end{bmatrix}$$

$$\begin{bmatrix} M_{\Delta} \\ n_1^T \\ n_2^A \\ n_2^T \\ n_2^T \end{bmatrix}$$

$$\begin{bmatrix} M_{\Delta} \\ n_1^T \\ n_2^A \\ n_2^T \\ n_2^T \end{bmatrix}$$

$$\begin{bmatrix} n_1^A \\ n_1^T \\ n_2^A \\ n_2^T \end{bmatrix}$$

$$\begin{bmatrix} K_{CPL} & O & K_{CPL} & O \\ O & O & O & O \\ K_{CPL} & O & K_{CPL} & O \\ K_{CPL} & O & K_{CPL} & O \\ O & O & O & O \end{bmatrix} \begin{array}{c} n_1^A \\ n_2^A \\ n_2^A \\ n_1^A & n_1^I \\ n_2 & n_2 \end{array}$$
(9b)

and recognizing the partitions belonging to each of the substructures, Eq. (4) may be written as

$$\left\{ \left[\frac{m_1}{o} \frac{1}{m_2} \frac{o}{m_2} \right] + \left[M_{\Delta} \right] \right\} \left\{ \frac{\ddot{\chi}_1}{\ddot{\chi}_2} \right\} + \left\{ \left[\frac{k_1}{o} \frac{1}{k_2} \right] + \left[K_{CPL} \right] \right\} \left\{ \frac{\chi_1}{\chi_2} \right\} = 0 \tag{10}$$

For each substructure defined by Eq. (1), a set of eigenvalues, $[\omega_i]$, and a set of mass normalized eigenvectors, $[\phi_i]$, can be obtained such that

Using the results from Eq. (11), we can now express Eq. (10) in terms of a set of generalized modal coordinates, $\{ \}$. The coordinate transformation

is given by

$$\{x\} = [\phi] \{g\}$$

$$n \times n \qquad n \times 1$$
(12)

where

$$\begin{bmatrix} \phi \end{bmatrix} = \begin{bmatrix} \phi_1 & | & o \\ \hline o & | & \overline{\phi_2} \end{bmatrix}$$

$$n \times n$$

$$(13b)$$

Substituting the transformation for $\{x\}$ into Eq. (10) and premultiplying by

$$\left[\phi\right]^{\mathsf{T}}$$
 yields

$$\left\{ \begin{bmatrix} \mathbf{I} \end{bmatrix} + \begin{bmatrix} \phi \end{bmatrix}^{\mathsf{T}} \begin{bmatrix} \mathsf{M}_{\Delta} \end{bmatrix} \begin{bmatrix} \phi \end{bmatrix} \right\} \left\{ \mathbf{\hat{g}}^{*} \right\} + \left\{ \begin{bmatrix} \omega_{i}^{*} & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} \phi \end{bmatrix}^{\mathsf{T}} \begin{bmatrix} \mathsf{K}_{\mathsf{CPL}} \end{bmatrix} \begin{bmatrix} \phi \end{bmatrix} \right\} \left\{ \mathbf{\hat{g}} \right\} = 0 \quad (14)$$

$$\mathsf{N} \times \mathsf{N}$$

Eq. (14) represents the most general form of the equation of motion for stiffness coupling. This equation is generally solved by partitioning the $\{q\}$ coordinates into two groups, kept and truncated. The truncated coordinates correspond to the high frequency substructure modes and are completely omitted from the equation of motion. Those degrees of freedom remaining, the partitioned set of kept coordinates, determine the final reduced size of the eigenvalue problem to be solved.

The general form of Eq. (14) may be simplified further by including the correct $\mathbf{m_{\Delta i}}$ partitions from Eq. (6) in each corresponding $[\mathbf{m_i}]$ at the substructure level. This is reasonable because we are assuming that there is no inertial coupling between substructures. This will result in $[\mathbf{M_{\Delta}}] = 0$ and Eq. (14) reduces to

$$\begin{bmatrix} I \end{bmatrix} \left\{ \ddot{\mathcal{F}} \right\} + \begin{bmatrix} K \end{bmatrix} \left\{ \mathcal{F} \right\} = 0 \tag{16}$$

where

$$\begin{bmatrix} \mathbf{K} \end{bmatrix} = \begin{bmatrix} \omega_1^{2} & 0 \\ 0 & \omega_2^{2} \end{bmatrix} + \begin{bmatrix} \mathbf{\Phi} \end{bmatrix}^{\mathsf{T}} \begin{bmatrix} \mathsf{K}_{\mathsf{CPL}} \end{bmatrix} \begin{bmatrix} \mathbf{\Phi} \end{bmatrix}$$

$$\mathsf{n} \times \mathsf{n} \qquad \mathsf{n} \times \mathsf{n} \qquad \mathsf{n} \times \mathsf{n}$$

After solving for the ω_i 's and ϕ_i 's, the only lengthy calculation left to be performed in order to obtain Eq. (16) is the matrix triple-product involving $\left[K_{\text{CPL}} \right]$. If we partition each $\left[\phi_i \right]$ row-wise in terms of its N_i^A and N_i^I coordinates such that

Eq. (13b) can be written as

$$\begin{bmatrix} \Phi \end{bmatrix} = \begin{bmatrix} \phi_1^A & o \\ \phi_1^I & o \\ o & \phi_2^A \\ o & \phi_2^I \end{bmatrix} \begin{pmatrix} n_1^A \\ n_2^A \\ n_2^A \\ n_2^I \end{pmatrix}$$

$$\begin{pmatrix} n_1^A \\ n_2^A \\ n_2^A \\ n_2^I \end{pmatrix}$$
(19)

where

$$\begin{bmatrix} \Phi^{A} \end{bmatrix} = \begin{bmatrix} \frac{\Phi_{1}^{A} \cdot O}{O \cdot \Phi_{2}^{A}} & n_{1}^{A} \\ O \cdot O \cdot \Phi_{2}^{A} & n_{2}^{A} \end{bmatrix}$$

$$(20b)$$

$$(n_{1}^{A} + n_{2}^{A}) \times N \qquad \underbrace{n_{1} \quad n_{2}}_{D}$$

$$\begin{bmatrix} k_{cpL} \end{bmatrix} = \begin{bmatrix} k_{cpL} + k_{cpL} \\ -\frac{1}{2} + \frac{1}{2} \\ k_{cpL} + k_{cpL} \end{bmatrix} n_{1}^{A}$$

$$(20c)$$

$$(n_{1}^{A} + n_{2}^{A}) \times (n_{1}^{A} + n_{2}^{A})$$

$$n_{1}^{A} \quad n_{2}^{A}$$

and the final form of [K] in Eq. (17) may be expressed as

$$[K] = \begin{bmatrix} \omega_1^2 & 0 \\ 0 & \omega_2^2 \end{bmatrix} + [\phi^A]^T [k_{CPL}] [\phi^A]$$

$$n \times n$$

$$n \times n$$
(21)

2.2 DYNAMIC TRANSFORMATION

As a result of omitting the higher substructure modes, the solutions from the truncated Eq. (16) will have errors introduced. The truncation errors can be greatly diminished by including the modes that would have been truncated through a dynamic transformation. Instead of truncating or omitting modes, all modes can be included through a transformation that relates the "reduced" modes not contained explicitly in the solution to the modes that are "kept." If Ω_i^2 corresponds to an exact eigenvalue of Eq. (16), the relationship between the eigenvalue and its eigenvector may be expressed in terms of the kept, Ω_i^2 , and reduced, Ω_i^2 , coordinates as:

$$\Omega_{i}^{2}\left[I\right]\left\{\frac{g^{k}}{g^{r}}\right\} = \left[\frac{K^{kk}}{K^{rk}}\right]\left\{\frac{K^{kr}}{K^{rr}}\right]\left\{\frac{g^{k}}{g^{r}}\right\}$$

$$\sum_{k=1}^{n} \left[I\right]\left\{\frac{g^{k}}{g^{r}}\right\} = \left[\frac{K^{kk}}{K^{rk}}\right]\left\{\frac{K^{kr}}{K^{rr}}\right\}\left\{\frac{g^{k}}{g^{r}}\right\}$$

$$\sum_{k=1}^{n} \left[I\right]\left\{\frac{g^{k}}{g^{r}}\right\} = \left[\frac{K^{kk}}{K^{rr}}\right]\left\{\frac{g^{k}}{g^{r}}\right\}$$

$$\sum_{k=1}^{n} \left[I\right]\left\{\frac{g^{k}}{g^{r}}\right\} = \left[\frac{K^{kk}}{K^{rr}}\right]\left\{\frac{g^{k}}{g^{r}}\right\}$$

$$\sum_{k=1}^{n} \left[I\right]\left\{\frac{g^{k}}{g^{r}}\right\} = \left[\frac{K^{k}}{K^{rr}}\right]\left\{\frac{g^{k}}{g^{r}}\right\}$$

$$\sum_{k=1}^{n} \left[I\right]\left\{\frac{g^{k}}{g^{r}}\right\}$$

where the $\{g^r\}$ corresponds to those modes previously truncated. If we designate N_{ℓ} as the total number of modes kept from all the substructures and N_{r} as the total number of modes reduced, then

$$N = N_{\ell} + N_{r} \tag{23}$$

Expanding Eq. (22) into two equations for some general frequency, $p^2 = \Omega_i^2$, yields

$$p^{2} \{ g^{k} \} = [K^{kk}] \{ g^{k} \} + [K^{kr}] \{ g^{r} \}$$

$$n_{k} = n_{k} = n_{k} = n_{k} = n_{r} = n_{r} = 1$$
(24a)

$$p^{2} \{ g^{r} \} = [K^{rk}] \{ g^{k} \} + [K^{rr}] \{ g^{r} \}$$

$$n_{r} \times 1 \qquad n_{r} \times n_{k} \quad n_{k} \times 1 \qquad n_{r} \times n_{r} \qquad n_{r} \times 1$$
(24b)

Solving Eq. (24b) for $\{q^k\}$ in terms of $\{q^k\}$ gives

where

$$[R] = -[K^{YY} - p^2I]^{-1}[K^{Yk}]$$

$$n_{YX}n_{K} \qquad n_{YX}n_{K} \qquad n_{YX}n_{K} \qquad (26)$$

Using Eq. (25) for some "reduction frequency", p, we can write

The dynamic transformation matrix, [T], is then defined as

$$\begin{bmatrix} T \end{bmatrix} = \begin{bmatrix} -\bar{I} \\ \bar{R} \end{bmatrix}$$

$$n \times n_{R} \qquad n \times n_{R} \qquad (28)$$

The reduced equation of motion is obtained directly by substituting the coordinate transformation

$$\left\{ g \right\} = \left[T \right] \left\{ g^{k} \right\}$$

$$\text{n.t.} \quad \text{n.t.} \quad \text{n.t.}$$

into Eq. (16) and pre-multiplying by the transpose of [T]. The reduced generalized mass and stiffness matrices can be written in the partitioned forms given by Eqs. (22) and (28):

$$[M^{k}] = [I] + [R]^{T}[R]$$

$$h_{k} \times h_{k} \quad h_{k} \times h_{k} \quad$$

$$[K^{\ell}] = [K^{\ell\ell}] + 2[K^{\ell r}][R] + [R]^{r}[K^{rr}][R]$$

$$n_{\ell} \times n_{\ell} \qquad n_{\ell} \times n_{\ell} \qquad n_{\ell} \times n_{r} \qquad n_{r} \sim n_$$

Conventional methods of determining eigenvalues may be applied to the reduced equation of motion to obtain a set of eigenvalues, $\begin{bmatrix} & & & \\ & & & \end{bmatrix}$, and a corresponding set of mass normalized eigenvectors, $\begin{bmatrix} & & & \\ & & & \end{bmatrix}$. From the coordinate relationship defined by Eq. (25), the reduced eigenvectors, $\begin{bmatrix} & & & \\ & & & \end{bmatrix}$, corresponding to the $\{q^{*}\}$ reduced coordinates are given by

$$[\gamma^{r}] = [R][\gamma^{k}]$$

$$n_{r} \times n_{k} \quad n_{r} \times n_{k} \quad n_{k} \times n_{k}$$
(31)

where

and the physical eigenvectors for the total solution will be given by

$$\begin{bmatrix} \Phi_{\chi} \end{bmatrix} = \begin{bmatrix} \Phi \end{bmatrix} \begin{bmatrix} \chi^{kr} \end{bmatrix}$$

$$n \times n_{k} \qquad n \times n_{k}$$
(33)

This solution will be exact for any Ω_i^* which is the same as the reduction frequency, ρ , used in developing [T].

Significant improvement can be obtained in the modes and frequencies by applying the Rayleigh-Ritz method in conjunction with the dynamic transformation for individual modes. This part of the dynamic transformation will be referred to as backsubstitution. For each Ω_i^k to be considered, a revised mode shape, $\lceil \tilde{k}_i^k \rceil$, can be determined by substituting $p = \Omega_i^k$ in $\lceil R \rceil$ and mass normalizing the mode shape:

$$[\aleph_i] = [\aleph_i] [\aleph_i^{\ell}]$$
(34a)

$$a_{i} = \left[\chi_{i}^{kr} \right]^{\mathsf{T}} \left[\chi_{i}^{kr} \right] \tag{34b}$$

$$NF_i = \sqrt{a_i}$$
 (34c)

$$\left[\overline{\gamma}_{i}^{kr}\right] = NF_{i}\left[\gamma_{i}^{kr}\right] \tag{34d}$$

where NF_i is the normalization factor used to mass normalize one S_i for some Ω_i^k .

A new estimate of \mathcal{L}_{i}^{k} will be given by

$$\overline{\Omega}_{i}^{k^{2}} = \left[\overline{y}_{i}^{kr}\right]^{T} \left[K\right] \left[\overline{y}_{i}^{kr}\right]$$

Another measure of the accuracy of the solution is provided by the change in the eigenvalues and is provided by the eigenvalue ratio defined as

$$\left(\bar{\Lambda}_{i}^{k}/\Lambda_{i}^{k}\right)^{2}$$
.

SECTION 3

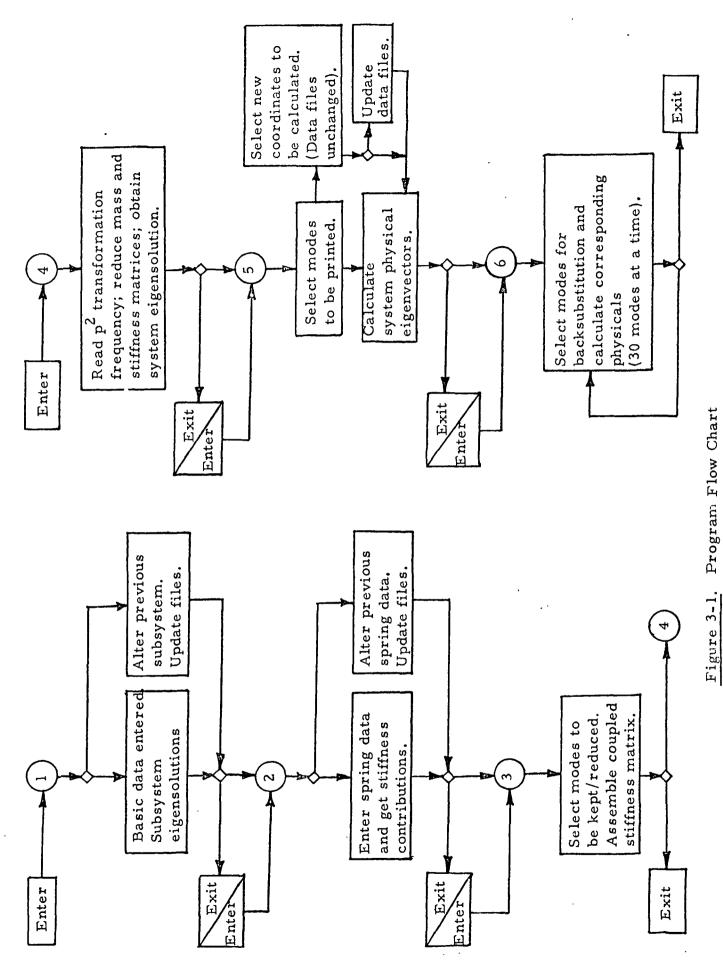
PROGRAM ENTRY POINTS

In order to provide user flexibility and at the same time minimize computation of basic data changes, six major entry points have been established for DAMUS:

- 1. Basic substructure data entered, subsystem eigensolutions.
- 2. Coupling spring stiffness data entered and stiffness contributions calculated.
- 3. Selection of modes to be kept/reduced/truncated, generalized mass and stiffness matrices calculated.
- 4. p value for dynamic transformation entered, eigensolution for system using the dynamic transformation.
- 5. Calculation of physical eigenvectors for total system.
- 6. Backsubstitution of selected modes from system solution.

Entry into the program is accomplished by designating a specific entry point (EP). Termination of the program is accomplished by designating the last EP the user desires to execute.

The Fig. 3-1 flow chart is included to show the general flow of the program. A corresponding flow chart showing the main Fortran subroutine called by the program may be found in Appendix B. The flow chart for input/output files required by the program at each EP is in Section 4. This flow chart corresponds in form to the one shown in Fig. 3-1.



3-2

A special vector input notation is used for reading in vectors used to select DOF orders. When it is required for the user to select a group of DOF's to be re-ordered or to designate a group of coordinates to be printed from a substructure, a vector of identifying DOF's is read into DAMUS by the READIM FORMA subroutine. The order in which the DOF numbers appear determines the particular sequence of DOF desired. If a sequential set of numbers from N1 to N2 is desired, the input may be abbreviated by the user. Inclusive groups of numbers to be generated in ascending order may be specified at any one time by using three elements of the input vector IV where

$$IV(I) = N1$$

$$IV(I+1) = 0$$

$$IV(I+2) = N2.$$

The integers from N1 to N2 will be sequentially expanded in the IV matrix starting from the IV(I) location. The last element of IV must be negative if this abbreviated form of input is used.

For an example, let us consider a substructure with 20 DOF's. It is desired to print only 10 of the substructure DOF's in a different order. The vector for reordering the DOF's would be designated as a 1 x 10 on the READIM header card. If the order to be printed is given as

then the shortened input vector would be given by

If all the DOF's were desired to be printed in their original order, the input vector (1X20) would be

1,0,-20

and the expanded vector of numbers 1 through 20 would be generated by the program.

Entry Point 1

The mass and stiffness matrices, $[m_i]$, $[k_i]$, for each substructure are read into DAMUS at EP-1. The substructures are defined in the program by a user supplied number which ranges from 1 to 20. Since each substructure is to be identified in the program by a distinct number, their input may be in any order. Input data for the mass matrix may be in two forms: an n x n square matrix or a l x n row vector. Before solving the substructure eigenproblem, the attachment coordinates must be identified and partitioned into the x, A set. An input vector IDDOF is used here to specify the N; A coordinates. Since the special input notation as previously described is to be used, only the n_i^A coordinates need be specified. The program will complete the vector for re-arranging the mass and stiffness matrices. The n, A coordinates must be partitioned in the same order as the coupling-spring DOF's. If one substructure couples to several others, then each set of attachment DOF's must be specified in the order in which they will be used. For example, assume that substructure i couples to 3 other substructures. The \boldsymbol{z}_{i}^{A} coordinates may then be partitioned as

$$\left\{\chi_{i}^{A}\right\} = \left\{\begin{array}{c} \chi_{i}^{AI} \\ \chi_{i}^{A2} \\ \end{array}\right\} \begin{array}{c} \eta_{i}^{AI} \\ \eta_{i}^{A2} \\ \end{array}$$

$$\left\{\chi_{i}^{A3}\right\} \begin{array}{c} \eta_{i}^{A3} \\ \end{array}$$

(If $\mathbf{x}_i^{A1} = \mathbf{x}_i^{A2}$, then only 2 partitions need to be specified). For EP-2, it will be necessary to input the \mathbf{n}_i^{A} locations since each spring only couples 2 substructures at a time. Thus, there will be at most, 3 sets of $\boldsymbol{\phi}_i^{A}$ associated with substructure i. After re-arranging the substructure DOF's, the complete vector will be printed out to allow the user to identify the substructure mode shapes. An additional input vector is required here to select which substructure DOF's are to be printed after the system is coupled. The DOF order desired refers to the original \mathbf{m}_i , \mathbf{k}_i , read into core, not the partitioned \mathbf{x}_i^{A} , \mathbf{x}_i^{I} coordinate set. If one desired all of the coordinates to be printed, the abbreviated vector $(1 \times \mathbf{n}_i)$ would be given by 1, 0, $-\mathbf{n}_i$ in the READIM format. An option is included at this point to rotate the \mathbf{m}_i , \mathbf{k}_i into system coordinates by reading in a 3 x 3 direction cosine matrix. The substructure may not be rotated if its size is not divisible by three.

Another option for EP-1 is one for altering or adding substructure data. The user may add new substructures at any time. If a substructure or group of substructures need to be altered, only those to be changed can be entered. The program tapes will be updated to reflect the changes without regenerating previous unaltered substructural data.

Coupling spring stiffness data is entered here. Each coupling spring stiffness matrix is associated with only 2 substructures. The user must specify which two substructures are being coupled, the number of attachment DOF's associated with each substructure, and the starting location of the n_i A; coordinates that were specified by the IDDOF vector in EP-1. The program then performs the product

$$\left[\Phi^{A} \right]^{T} \left[K_{CPL_{i}} \right] \left[\Phi^{A} \right]$$

and saves the result for assembly in EP-3 where the ϕ^A contains only those \mathbf{x}_i^{Ai} coordinates corresponding to the $\mathbf{K}_{\text{CPL}_i}$ DOF's. As in EP-1, the user may add additional coupling springs corresponding to more substructures added. If a substructure was altered, this EP must be executed again to reflect the substructures' altered eigenvector. Only those coupling springs of direct concern need be calculated. The program will update the tapes without regenerating previous unaltered substructure data.

At this EP, the user specifies which modes are to be kept and reduced. The input matrix KEEP (2 x MAXSUB) is used where the column corresponds to a substructure. The (1, i) location specifies the total number of lowest modes kept for substructure i and the (2, i) row specifies the total number of next highest modes to be reduced. All other modes will be truncated. The restrictions for the total kept and reduced modes are given by

$$\sum_{i=1}^{\text{MAXSUB}} \text{KEEP}(1,i) \leq 100$$

$$\sum_{i=1}^{\text{MAXSUB}} KEEP(2,i) \leq 200$$

The generalized stiffness matrix is then assembled in its kept and reduced partitions. There must be at least 2 modes kept from each substructure read into DAMUS. For KEEP(1,i) = 10 and KEEP (2,i) = 20, the program will select modes 1 to 10 for the kept partition from substructure i and will place modes 11 to 30 in the reduced partition.

Entry Point 4

The reduction frequency, p, is entered at EP-4, and the dynamic transformation is applied to obtain the reduced mass and stiffness matrices.

The eigenvalues for the coupled substructures are now obtained.

This entry point calculates the coupled physical eigenvectors* which are printed in substructure groups. The order in which they are to be printed is determined by the order the substructures were originally read into DAMUS. The user must specify how many modes are to be printed by specifying the first and last mode number of the group of modes desired. Considerable computer time may be saved by selecting coordinates and printing a few of the modes since only those selected will be calculated. The user may desire to re-enter the program to select new coordinates to be printed or more modes. If the option to obtain new coordinates is selected, the user must specify which substructures will be printed and a new identification vector for selecting the coordinates for each substructure being considered. When selecting only different modes to be printed, those coordinates previously defined in EP-1 will be used to calculate physicals. An option also exists for making the coordinate selection a permanent change and will cause the basic program tapes to be updated to reflect any new ordering specified by this entry point. The order in which the substructure groups will be printed may be altered this way.

*Referred to as "physicals" for convenience.

This EP is for backsubstitution. The user may select in any order up to 30 modes at a time to be backsubstituted. The same physicals as specified in EP-5 will be calculated and printed. If the program is entered here, it will use the system tapes previously generated and saved to calculate the physicals. For new coordinate selection in EP-5, the correct save tape must be used to obtain the physicals. If EP-6 is executed after EP-5 and a new coordinate selection was made, the physicals calculated will be those currently specified in EP-5. The new eigenvalues will be printed along with the normalization factor used to mass normalize the vectors and the frequency ratio $(\Omega_i^k/\Omega_i^k)^2$ used as a measure of the frequency change.

SECTION 4

INPUT/OUTPUT DATA

4.1 INPUT DATA

This section describes the necessary input data required to execute DAMUS and is ordered by entry points. The data cards and the variables appearing on them are listed in sequential order with the input format or FORMA subroutine specified. The definitions for the variables specified on the cards are given to clarify their meaning.

Input Data for Starting Program

No.	Input Order	Format
1	IRUNNO, UNAME	(A6, 4X, 3A6)
2	TITLE 1	(12A6)
3	TITLE 2	(12A6)
4	FOD	(E10.0)
5	NTAPE(1), $NTAPE(2)$,, $NTAPE(12)$	(1215)
6	IENTR, IEXIT	(215)

Definitions

IRUNNO	=	Run No.
UNAME	=	User's Name
TITLE 1	=	First Title
TITLE 2	=	Second Title
FOD	Ξ	Final off-diagonal value for diagonalizing a matrix [A] using the method of Jacobi.
NTAPE(I)	=	Twelve tape and/or file units used by the program and assigned by the user. Only those tapes actually used must be specified.
IENTR	=	Entry Point for entering program. There are 6 entry points in all defined by the integers from 1 to 6. If the program is being entered at Entry Point 1 other than the first time, then IENTR = -1 must be specified.
IEXIT	=	Exit Point for terminating the program. The exit points are identical to the entry points with program termination occurring after the execution of the entry point specified by IEXIT.

4. l. l Input Data - Entry Point 1

Card No.	Input Order	Format
1	NSUBS, IOP	(215)
2	ISUB, KEPMOD, MOPT, IROT	(415)
3	IDDOF (1XN1)	READIM
4	K (NXN)	READ
5	M (NXN) or (1XN)	READ
(6)*	RCOS (3X3)	READ
7	IPDOF (1XN2)	READIM

Cards 2 through 7 are repeated for each substructure defined.

Definitions

NSUBS	=	Number of substructures to be read into program at this time. There will be NSUBS sets of cards from 2-7 following Card 1.	
IOP	=	0 denotes the first time the program is entered at Entry Point 1	
	=	denotes more substructures are to be added to a set of substructures previously defined	
	=	2 denotes one or more substructures from a previously defined set are to be changed.	
ISUB	=	Substructure identification number which ranges from 1 to 20. Each substructure must be identified by a different no.	
KEPMOD	=	by a different no. Total number of modes to be saved on tape for substructure "ISUB." This number must not be less than the sum of the number of modes to "kept" plus the number of modes to be "reduced" for this particular substructure.	

^{*()} denotes optional input data and is not required if option is not exercised.

1 Mass matrix is square NXN MOPT 2 Diagonal mass matrix to be read in as a = lXN vector. **IROT** 0 Substructure already in system coordinates. Delete Card 6 from input. 1 Rotate substructure by direction cosines, a 3X3 matrix, read in on Card 6. **IDDOF** Special IXN1 integer vector used to place connecting coordinates in first N1 DOF locations for "ISUB." Order of connecting DOF's must correspond to those used in coupling spring. The order in which the DOF's appear in IDDOF determines the rearranged DOF order. N1 = the number of elements in IDDOF. K Input Stiffness Matrix, for "ISUB". (NXN) Input Mass Matrix for "ISUB". (NXN) or (1XN) M = R COS Optional Direction Cosines Matrix (3X3). Total number of substructure DOF's must be divisible by 3 in order to exercise this option. Special 1XN2 integer vector used to select those **IPDOF** physical coordinates to be calculated from "ISUB". The order in which the DOF's appear in IPDOF will determine the order in which they will be printed for substructure "ISUB." If no physical coordinates from "ISUB" are to be calculated, IPDOF(1) must equal zero. N2 equals the number of elements in IPDOF. All substructure DOF numbers refer to the original order in which they were read into the

computer.

4.1.2 Input Data for Entry Point 2

Card No.	Input Order	Format
1 2	NCPLS, IOP ISUB1, NROW1, NS1, ISUB2,	(2I5) (6I5)
3	NROW2, NS2 KCPL (NXN)	READ
	<u>Definitions</u>	
NCPLS	Number of coupling springs program at this time. There sets of cards 2-3 following	e will be NCPLS
IOP	= 0 denotes the first time that Entry Point 2.	
	= 1 denotes more coupling to a set of data previous	
	= 2 denotes one or more co previously defined set a changed.	upling springs from a
ISUB1	= First substructure coupled	ov spring (ISUB no.)
NROW1	= Number of connecting DOF's particular spring.	· •
NS1	= Starting DOF location of coowere ordered by IDDOF. Thave more than one set of constitution of coordinate the reordered set of DOF's.	he substructure may onnecting coordinates.
ISUB2	= Second substructure coupled ISUB2 must always be great	
NROW2	= Number of connecting DOF's particular spring.	
NS2	= Starting DOF location of coowere ordered by IDDOF.	rdinates in ISUB2 which
KCPL	Coupling spring stiffness material to ISUB2. DOF's for coupling order as specified for the ISUB IDDOF with the ISUB I confirst. N is the size of the total inates used from each substitute.	ng spring are in same UB1, ISUB2 coordinates ordinates appearing otal number of coord-

4.1.3 Input Data for Entry Point 3

Card No.	Input Order	Format	
1	KEEP (2XMXSUB)	READIM	

Definitions

KEEP

INTEGER Matrix defining how many modes are to be kept and reduced for all of the substructures. The KEEP(1, I) row defines the number of low modes to be kept for substructure I. The KEEP (2, I) row defines the number of modes to be reduced for substructure I. Modes from the substructures are arranged in ascending order by frequency. For some substructure ISUB, the first KEEP(1, ISUB) modes will be kept and the next KEEP(2, ISUB) modes will be reduced by the dynamic transformation.

MXSUB is the highest numbered substructure read into the program. A zero in some KEEP(2, ISUB) location will include all modes in the kept set.

4.1.4 Input Data for Entry Point 4

Card .		
No.	Input Order	Format
1	LAMDAO (1X1)	READ

Definitions

LAMDAO = p² value used for the dynamic transformation for reduction.

4.1.5 Input Data for Entry Point 5

Card <u>No.</u>	Input Data	Format
1	MD1, MD2, IOP	(315)
(2)*	ID (1XN1)	READIM
(3)*	IPDOF (1XN2)	READIM

There will be N1 Card (3)'s.

Definitions

MD1 MD2	=	Mode number of first mode to be printed. Mode number of last mode to be printed.
IOP	=	<pre>0 no optional cards needed 1 requires cards (2) and (3), but data files not updated 2 requires cards (2), (3) with permanent update</pre>
ID	=	of files. An integer vector containing Nl substructure ID's for which new physical DOF's are to be defined.
IPDOF	=	Ordering vector for selecting DOF's from each substructure defined by ID. There will be N1 of these cards.

^{*()} Indicates optional data and is not required if option not exercised.

4.1.6 Input Data for Entry Point 6

No.	Input Data	Format
1	NBKSB	I5
2	IMODE (1XNMD)	READIM

Definitions

NBKSB	=	Number of groups of modes to be backsubstituted. 30 modes may be specified to be backsubstituted at any one time. NBKSB tells the program how many groups of 30 modes are to be selected.
IMODE	=	Integer vector selecting modes to be backsubstituted with NMD ≤ 30. There will be NBKSB card (2)'s.

4.2 OUTPUT FILES/TAPES

This section describes the data saved on each logical file. Figure 4-1 presents a Tape Flow Chart indicating which files will be required for executing the desired entry points. The program is written to handle files instead of tapes. A computer utility program should be used to save the necessary files on tape for re-entry into DAMUS. All eigenvalues and eigenvectors are output by subroutine WTAPDS and may be read by RTAPDS for use in another program.

Figure 4-1. Tape Flow Chart

4.2.1 Description of Output Files/Tapes (Ref. Fig. 4-1)

NTAPE(I)	Description
I	
1	This tape contains basic data necessary for program logic. It includes substructure sizes, ordering data, coupling indices, and data locations on the various tapes. It is required for every Entry Point (EP) and will be updated to reflect any changes due to option selections. It consists of one logical record written in binary by the standard Fortran WRITE routine.
2	This tape contains the eigenvalues and eigenvectors for each substructure. In addition, it has the identification vectors used to re-order the substructure DOF's for the initial solution and for printing physicals. This tape is output data from EP-1 and is used by EP-2, 3. If IOP = 2 for EP-5, this tape is needed as input. A new NTAPE(2) will be output on NTAPE(12) for subsequent runs.
3	This tape contains the partitioned set of substructure eigenvectors to be used in calculating physical vectors. Those DOF's to be calculated are packed into 100 DOF blocks and saved in the order read in. This is output from EP-1 and is required as input for EP-5 and EP-6, only if IOP = 0 for EP-5.
4	This tape contains the partitioned coupling spring data used for assembling the generalized stiffness matrix. The substructures are coupled 2 at a time. This tape is output from EP-2 and is required input for EP-3.
5	This tape contains the assembled generalized stiffness matrix in partitioned form plus the eigenvalues and participation factors from the system solution. Data is output from EP-3 and EP-4 on this tape and is required as input for EP-5 and EP-6. Re-entry into the program at EP's 3 and 4 will destroy previously generated data for that particular EP. If it is desired to save the previous data for some future reference, a new tape should be used; i. e., copy old tape data to new tape and use if data from EP-3 is needed.

NTAPE(I)	Description	
ĭ		
6	This is a scratch file. It is basically required only for EP-4. For particular options, it may be required for EP's 1,2,5, and 6. If IOP > 0 in EP-5, NTAPE(6) replaces NTAPE(3) for EP-5,6. If IOP = 2 in EP-5, several files are updated permanently; and NTAPE(6) should be saved and used as NTAPE(3) for subsequent runs.	
7	This is a scratch file required for EP-4. If IOP > 0 for EP-5, it is required there as a scratch file also.	
8	This is an output tape containing only the system physical eigenvectors which are partitioned by substructure from EP-5.	
9	This output tape contains those selected system eigenvalues and eigenvectors obtained for backsubstitution from EP-6.	
10	Special input tape for EP-1 when IOP = 2. Use previous NTAPE(2) data and new NTAPE(2) generated. NTAPE(7) may be used here if old NTAPE(2) copied onto this file.	
11	Special input tape for EP-2 when IOP = 2. Use previous NTAPE(4) data and new NTAPE(4) generated. NTAPE(7) may be used here if old NTAPE(4) data copied onto this file. If NTAPE(7) used in EP-1 for NTAPE(10), it may not be used again for EP-2 if the EP's are being executed consecutively.	
12	Special output tape for EP-5 when IOP = 2. This tape replaces NTAPE(2) for subsequent runs.	

4.2.2 Data Locations on Tapes

	Location	Matrix	
I			
1	1		Basic data
2	1	IDDOF	Vector for reordering substructure DOF's
	2	LAMDA	Substructure eigenvalues
	3	PHYSUB	Substructure eigenvectors
	4	IPDOF	Vector for selecting substructure DOF's to be printed in physicals.
	• • •		Set repeated for as many substructures read into program.
3	1	PHYPRT	Partitioned set of substructure vectors assembled by IPDOF.
	• • •		Repeated in blocks of 100 DOF until finished.
4	1	CPLII	Partitioned coupling spring, CPL.
-	2	CPL22	rarranca coap-ing spring, or 2.
	3	CPL12	
	• • •)	Set repeated for each spring read into program.
5	1	K22	Partitioned stiffness matrix for reduced coordinates
	2	K12-1	Partitioned stiffness matrix coupling terms
	3	K12-2)	
	4	K11	Partitioned stiffness matrix for kept coordinates
	5	LAMSYS	System eigenvalues
	6	GAMK	Participation factors for kept coordinates
	7	GAMR 11	Participation factors for reduced coordinates in partitioned form.
	8	GAMR 12	•
6	1	M*	Reduced mass matrix
-	2	2K12*R11	
	3	2K12*R12	
	4	K 2 2*R11	Partitioned multiplications
	5	K22*R12	

	Location	Matrix	
7	1	R11	R matrix for dynamic transformation
	2	R12	in partitioned form.
8	1	PHYSYS	System Eigenvectors One record for each substructure.
9	1 2 	LAMBKS PHYBKS	Eigenvalues from backsubstitution Eigenvectors from backsubstitution Repeat set for as many modes selected in groups of 30.
10		Optional in	nput tape, NTAPE(2)
11		Optional in	uput tape, NTAPE(4)
12		Optional or	utput tape, NTAPE(2)

APPENDIX A

FORTRAN LISTING OF DAMUS AND FLOW CHARTS

This appendix contains the Fortran listing of DAMUS. The main program has been divided into four links with each link beginning with one of the six entry points. The main program calls the first link with all links being called in sequential order.

Link	Entry	Subroutine
No.	Point	Name
1	1	STCl
2	2	ST C2
3	4	STC4
4	6	STC6

The flow chart following the program listing shows the major subroutines called by the main program links. If the subroutine called requires input data, a flow chart for that particular subroutine has been included.

01 06=06-73 15.547	STC MAIN LINK
CSTC STC COMMON TENTR 1; COMMON ZNLIN	MAIN LINK ,IEXIT,FOD,NUT1,NUT2,NUT3,NUT4,NUT5,NUT6,NUT7,NUT8 NUT9,NUT10,NUT11,NUT12 EZ/ DUMY1 /LSTART/ DUMY2(30)
CALL FINK FACTHM = SOO COMMON AMOUSE	VC/ LNG1HW, W(200)
ĒŅD	
23747 WORDS OF MEMORY US	ED BY THIS COMPILATION
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5=06-73 15.549 SIIFENESS COUPLING ENTRY 1
                STIFFNESS COUPLING ENTRY 1
CSTC1
       SUBROUTINE STC1
       DIMENSION A(100,100);S$130,100),PHY(100,100)
                 ID(100), IV(100), JV(100), T1(100), T2(100), T3(100)
                 NNDOF(20,6),KEEP(2,20),KCPL(210),KSR(20),KSR(20)
      3.
                 IDP4Y(21), IDCP (100), PHD(20)
       COMMON LENTR, LEXIT, FOD. NUT1, NUT2, NUT3, NUT4, NUT5, NUT6, NUT7, NUT8
                   NUTS, NUT10, NUT11, NUT12
      COMMON /NLINEZ/ DUMY1 /LSTART/ DUMY2(30)
       COMMON INDRKVC/ LNGTHW: N(200)
       DATA KD1, KD2, KD3, KD4, KD5, KD6, KD7, KD8/100, 200, 2, 20, 300, 21, 6, 100/
       DATA | 1 1 1 | 2 | 3 | 4 | 6 | 5 | 6 | 7 | 7 | 6 | 6 | 10 | 11 | 11 | 12 | 11 * 1000 |
       DATA PHO(1)/120HPH71 PHY2 PHY3 PHY4 PHY5 PHY6 PHY7 PHY6
           PHY10 PHY11 PHY12 PHY13 PHY14 PHY15 PHY16 PHY17 PHY18 PHY19 PH
      $Y9
      $Y20 /
       DATA NSUBT, NOPLY, NNDOF, IDPHY, IDCPL, KCPL, KEEP, KSK, KSR/533*0/
 1JC0 FORMAT (1615)
 1001 FORMAT (510.0)
 2000 FORMAT (///tox+FOD =+,1PE12,4)
 2001 FORMAT (///10x17HINPUT TAPE NOS, =,1215,/10x17HUNIT ASSIGNED
                   1215)
     1.
 2002 FORMAT (///104 IENTR = 15,10X IEXIT = 15)
 2003 FORMAT (///10x'ENTRY POINT'I5,4X'HAS BEEN COMPLETED.')
 2004 FORMAT (///10X! IENTRY = 115,10X! NSUBS = 115,10X! IOP = 115)
       CALL START
       READ (5,1301) FUD
             (5.1000) N.JTB, NIJT1, NUT6, NUT2, NUT3, NUT4, NUT5, NUT7, NUT9
       READ
                   NUT15,NUT11,NUT12
             (5,1000) LENTR, LEXIT
       READ
       WRITE (5,2000) FOD
      WRITE (6,2001) (1,1=1,12), NUT3, NUT1, NUT6, NUT2, NUT3, NUT4, NUT5, NUT7
                   UUT9; NUT10, NUT11, NUT12
      WRITE (6,2002) IENTR, IEXIT
       IF (!ENTR.GT.1) GO TO 9002
       IF (IENTR.EQ.1) GU TO 9001
       REWIND NUTS
       READ (NUTS) NSUBT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK
                  KSR:N:M:M1.M2.M1P1.NSYM:MSYM
                   IENTRY = 1
 9001
  GET SUBSTRUCTURE MODAL DATA FROM MASS AND STIFFNESS MATRICES
      READ (5,1000) NSUBS, IOP
       CALL PAGEND
       WRITE (6,2004) LENTRY, NSUBS, TOP
       [F ([OP.EQ.2) GOTTO 120]
       CALL SUBDAT (IOP.A.S.PHY.NNDOF.IDPHY.ID.IV.JV.T1.T2.T3
                   NSUBS, NSUBT, KD1, KD4, KD1, KD6, LL1, NUT1, LL6, NUT6, FDD, PHD)
      60 T) 125
      NSUBT = 0
```

	#05-73 15.549 STIFFNESS COUPLING ENTRY 1
•	CALL SUBDAT (IOP:A.S.PHY, NNDOF, IDPHY, ID, IV, JV, T1, T2, T3 1. NSUBS, NSUBT, KD1, KD4, KD1, KD6, LL4, NUT4, 0, 0, FOD, PHD) CALL DELSUB (A.PHY, NNDOF, IDPHY, ID, IV, JV, NSUBS, NSUBT, KD1, KD2, KD7, 4 1. LL1, NUT1, LL6, NUT6, LL10, NUT10, LL4; NUT4, NUT8) 125 REWIND NUT8
	WRITE (NUTS) MSUBT, NNDOF, MCPLT, LOCPL, KCPL, LOPHY, KEEP, KSK 1. KSR, N, M, M1, M2, M1P1, NSYM, MSYM
•	CALL EOF3 (LL1, NUT1, LL6, NUT6, LL8, NUT3) CALL PRINTI (31HSUBSTRUCTURES READ INTO PROGRAM, 6, NNDOF(1, 6) 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	TIF (TEXIT, EQ. TENTRY) GO TO 9990
	9002 CALL LINK (6HENTRY2)
	9990 CALL PAGEHD WRITE (6,2003) IENTRY STOP
	END
+	WORDS OF MEMORY USED BY THIS COMPILATION
	·

A-4

.

```
STC2
6=06-73 15.554
CSTC2
                   STCS
        SUBROUTINE STC2
        DIMENSION A(100,100); S(100,100), PHY(100,100)
                    $12(100,200),59(20100)
       1
2
                    IV(100), JV(100), KKPT(100,2), KRED(100,2), MRED(2), MKPT(2)
      3.
                    NUDGF(20,6), KEEP(2,20), KCP, (210), KSK(20), KSR(20)
                    IDPHY(21), IDCPL(100)
        COMMON TENTR, JEXIT, FOD, NUT1, NUT2, NUT3, NUT4, NUT5, NUT6, NUT7, NUT8
                      NUT9, NUT10, NUT11, NUT12
        COMMON /ILITEZ/ DUMY1 (LSTART/ DUMY2(30)
        COMMON /YORKYC/ LNGTHW.W(200)
        EQUIVALENCE (SS(1),S(1,1)), (SS(1),S12(1,1)), (SS(10001),PHY(1,1))
        DATA KD1, KD2, KD3, KD4, KD5, KD6, KD7, KD8/100, 200, 2, 20, 300, 21, 6, 100/
        DATA LE1, LL2, LL3, LL4, LL5, LL6, LL7, LL9, LL10, LL11, LL12/11*1000/
 1000 FORMAT (1615)
2003 FORMAT (/// UX'ENTRY POINT' 15,4X'HAS BEEN COMPLETED.')
2006 FORMAT (///IOX'IENTRY = 15,10X'NCPLS = 15,10X'IOP = 15)
  2007 FURGAT (///10X:IENTRY =115)
        REVIND NUTS
               (NUTS) "SUBT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK
      KSR. W. H. M. M. M. P. INSYM. MSYM
GO TO (9002,9002,9003,9004,9004,9004), IENTR
                      IENTRY = 2
 9002
C
    GET INDIVIDUAL K& CONTRIBUTIONS FROM COUPLING SPRINGS
       READ (5,1000) NCPLS, 10P
        CALL PAGEND
        WRITE (6,2006), IENTRY, NCPLS, IOP
        IF (10P.E0.2) GO TO 210
        CALL CPLSPG (A.S.PHY, NNDOF ; KCPL, IDCPL, NCPLS, NCPLT, KD1, KD1, KD4
                      LL2, NUT2; LL1, NUT1)
        IF (IEXIT.EQ. IENTRY .DR. IOP.EQ. 1) GO TO 220 GO TO 230
       NCPLT = 0
  210
       CALL CPLSPG (A,S,PHY,NNDOF,KCPL, IDCPL,NCPLS,NCPLT,KD1,KD1,KD4
                      LE4, NUT4; LL1, NUT1)
      1.
             DELCPL (A, NIDOF, IDCPL, KCPL, IV, NCPLS, NCPL T, KD1, KD2, KD7, KD8, KD
                      LL2, NUT2, LL11, NUT11, LL4, NUT4, NUT8)
       REWIND NUTS
        WRITE (NUTS) NSUBT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK
                      KSR, N. H. M. A. H. P. I. NSYM. MSYM
(EL8, NUT8, 0, 0, 0, 0)
        CALL FOF3
        CONTINUE
 530
        CALL EOF3
                      (LE2, NUT2, 0, 0, 0, 0)
             CNNCTV (A, NNDOF; KCP, , KD4, KD1, KD4)
           (TEXIT.EQ. TENTRY) GO TO 9990
                      TENTOY = 3
 9003
    K* ASSEMBLY
```

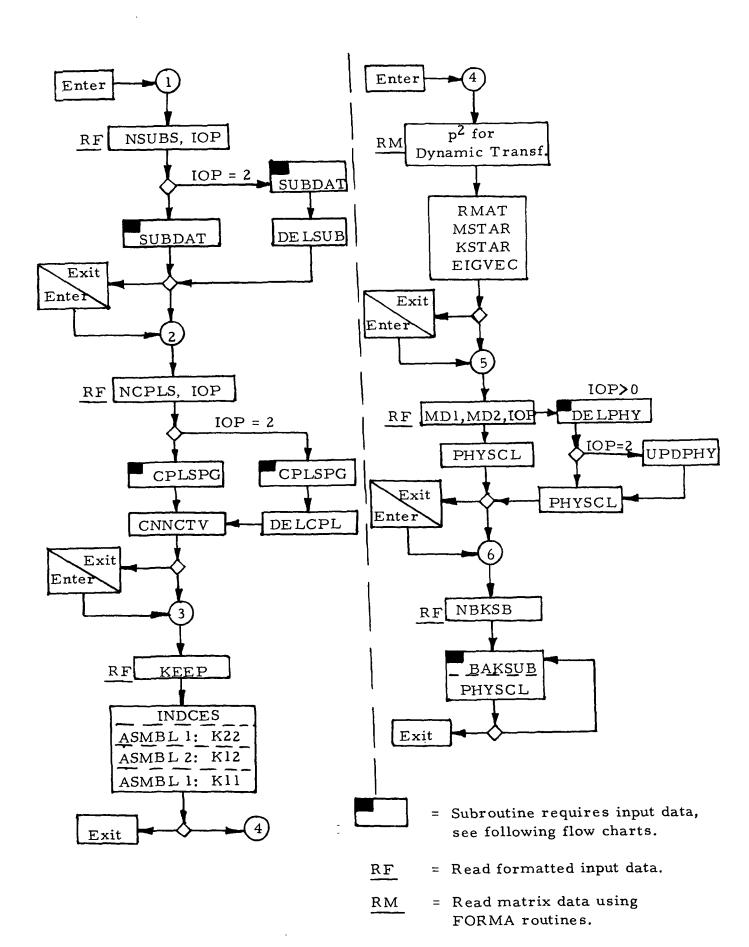
=0 <u>6-73</u>	15,554	STC2
C		
	ALL PAGEND	TENTEN
	RITE (6,20) Ali READIN	(KEEP,NR,MXSUB,KD3,KD4)
C)	ALL INDCES	(KEEP, MXSUB, KSK, KSR, N, M, NSM1, M1, M2, M1P1, NSYM, MSYM, KD3
		VSUBT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK
1.	an de dessa elegado de spale.	KSR, N. M. M1 . M2 . M1P1 . NSYM . MSYM
cc,	ALL EOF3	(LL8, NUT8, 0, 0, 0, 0)
-	MBLE K22*	
~ /	ALL ACMBIL	(2,55,4,KRED,MRED,KEEP,NNDOF,KSRTKCPL,IV,JV,M,MXSUB
1.	in many 2 in in the T	NSM1, MSYM, KD1, KD3, KD4, 1, LL3, NUT3; LL2, NUT2, LL1, NUT1)
C ASSE	MBLE K12*	
ر ادر است.	ALL ASMRIZ	(S12, A, KKPT, MKPT, KRED, MRED, KEEP, KSK, KSR, KCPL, IV, JV, N,
4.0	, m, m, F, W 147 be Ca	M1, M2, M1P1, MXSUB, NSM1, KD1, KD3, 2, LL3, NUT3, LL2, NUT2)
C	MOLE VAAA	
C ASSER	MBLE K11*	
	ALL ASMAL1	(1,55,A,KKPT,MKPT,KEEP,NNDOF,KSKTKCPL,IV,JV,N,MXSUB
1,		NSM1,NSYM,KD1,KD3,KD4,4,LL3,NUT3;LL2,NUT2,LL1,NUT1)
		(LL3,NUT3,0,0,0,0) R.IENTRY) GO TO 999 ₀
C	. (152VI.)	4.17.1417 do 10 10 10
•	ALL LINK	(6HENTRY4)
C oogn r	ALL PAGEHD	The state of the s
	RITE (6,20)	33) IENTRY
	TOP	
E	ND	
พฎกฎร of	F MEHORY U	SED BY THIS COMPILATION
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	and the last control of the state of the sta	

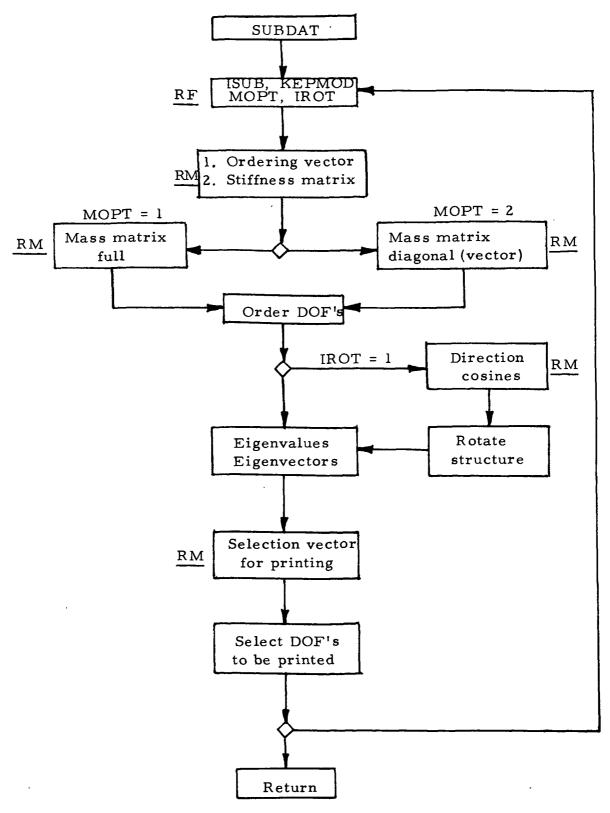
-		
		1
		A-6

```
STIFFNESS COUPLING ENTRY 4
-06-73 15.558
CSTC4
                STIFFNESS COUPLING ENTRY 4
      SUBROUTINE STC4
      DIMENSION A(150,100), S(100,100), PHY(100,100) TS12(100,200)
                 S21(200:100).R(200:50).R2(200:50).SS(20:00)
                 ID(100), tv(100), Jv(100), T1(100), T2(100), T3(100)
                 MNDOF(20,6), KEEP(2,20), KCP, (210), KSK(20), KSR(20)
     3,
                 IDPHY(21), IDCPL(100), PHD(20)
                 LAMSYS(1JU)
             IENTR, IEXIT, FOD, NUT1, NUT2, NUT3, NUT4, NUT5, NUT6, NUT7, NUT8
NUT9, NUT10, NUT11, NUT12
     COMMON INLINEZ/ DUNY1 /LSTART/ DUMY2(30)
      COMMON /WORKYC/ LNGTHW, W(200)
      EQUIVALENCE (SS(1),S(1,1)), (SS(1),S12(1,1)), (SS(1),S21(1,1))
                 (\Lambda(1,1), R(1,1))
     1.
                 (SS(10001), pHY(1,1)), (SS(10001), R2(1,1))
      REAL LAMSYS, LAMDAQ
      DATA_KD1,KD2,KD3,KD4,KD5,KD6,KD7,KD8/100,200,2,20,300,21,6,100/
      DATA LL1, LL2, LL3, LL4, LL5, LL6, LL7, LL9, LL10, LL11, LL12/11*1000/
      DATA PHD(1)/120HPHY1 PHY2 PHY3 PHY4 PHY5 PHY6 PHY7
          PHY10 PHY11 PHY12 PHY13 PHY14 PHY15 PHY16 PHY17 PHY18 PHY19 PH
     SY20 /
 1000 FORMAT (1615)
 2003 FORMAT (///<sub>10</sub>X'ENTRY POINT'I5,4X'HAS BEEN COMPLETED.')
2005 FORMAT (///10X'IENTRY = 15,10X'MD1 = 15,10X'HD2 = 15,10X'IOP = 15)
2007 FORMAT (///10X IENTRY = 115)
      REWIND NUT8
      READ (NUT8) MSUBT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK
                  KSR, N. H. M1. M2. M1P1. NSYM, MSYM
     GO TO (9004,9004,9004,9004,9005,9006), LENTR
                   IENTRY = 4
 9004
C FORM R FOR DYNAMIC TRANSFORMATION
      CALL PAGEHD
      WRITE (6,2007) IENTRY
      CALL READ
                 (LAMDAO, NR, NC, 1, 1)
      CALL RTAPSS (SS. HR. NC. ANM. 1, LL3, NUT3)
      CALL RMAT (SS.R.LAMDAO, M.KD2.1.LL5.NUT5.2.LL3.NUT3)
C
      CALL MSTAR (A.S21.N.M.M1P1.KD1,KD2,1,LL4,NUT4,1,LL5,NUT5)
      CALL KSIAR (S127R.SS.S.A.R2, N.M.M1P1, KD1, KD2, 2, LL4, NUT4
2, LL3, NUT3, 1, LL5, NUT5, 1, LL3, NUT3)
   SOLVE FOR EIGENVALUES AND EIGENVECTORS
      CALL EIGVEC (A, 5, S21, LAMSYS, T2, T3, N, M, M1, M2, M1P1, KD1, KD2
```

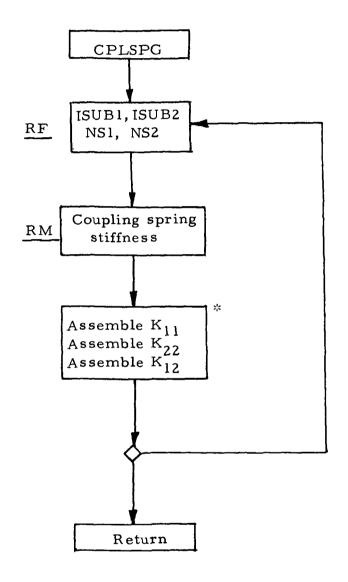
=06 - 73 15.553	STIFFNESS COUPLING ENTRY 4
1.	5,LL3,NUT3,1,LL4,NUT4,1,LL5,NUT5;FOD)
CALL EOF3	(LL3; NUT3; 0; 0; 0; 0) 10. IENTRY) GO TO 999
9005 C	IENTRY = 5
READ (5.10	00) MD1,MD2,IQP
CALL PAGEHO WRITE (6.20	105) IENTRY,MD1,MD2,IOP
IF (IOP.EQ.	0) GO TO 520
CALL DELPHY	(A,PHY,NNDOF,IDPHY,T ₁ ,ID,IV,JV,NSUBS,KD ₁ ,KD4,KD6
IF (10P.E0.	1) GO TO 510
CALL UPDPHY	T(A,NNDOF,JV,NSUBS,NSUBT,KD1,KD4,LL12,NUT12,LL1,NUT1 LL5,NUT5)
REWIND NUTS	
) 'ISURT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK KSR, N, M, M1, M2, M1P1, NSYM, MSYM
CALL EOF3	(LL4, NUT4, LL8, NUT8, LL12, NUT12)
5 ₁ 0 LL6 = LL4 NUT6 = NUT4	
i ngagagan in an matalah kalaman ini ini ngangan an minin matalah dalah dalah dalah ga Y	
GET PHYSICALS	
520 CONTINUE	
CALL PHYSCL	(PHY,S,A,R,NNDOF,KEEP,KSK,KSR;IDPHY,N,MD1,MD2,KD1 KD2,KD4,KD3,KD6,1,LL7,NUT7,6,LL3,NUT3,LL6,NUT6,PHD)
CALL EOF3	(LL7) NUT7, arning)
IF (IEXIT E	7. (ENTRY) GO TU 9890
9006 CALL LINK	(SHEUTRYS)
9990 CALL PAGEHD	
WRITE (6,20	
STOP END	
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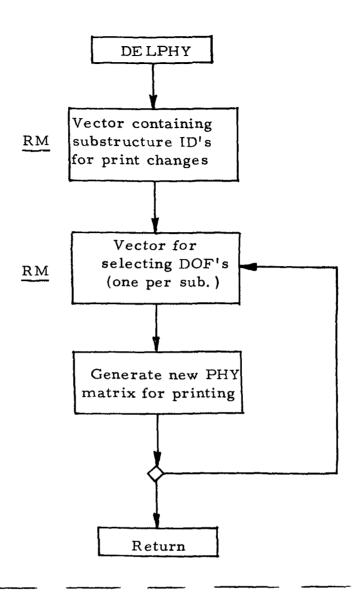
```
6-06-73 15.562 STC6
CSTC6
                STC6
       SUBROUTINE STO6
       DIMENSION A(100,100),S(100,100),PHY(100,100)7512(100,200)
                 S21(200,100), GAMA(300,30), SS(20100)
                 10(100),[v(100),Jv(100),T1(100),T2(100),T3(100)
                 NNDOF(20,6), KEEP(2,20), KCPL(210), KSK(20), KSR(20)
                 IDPHY(21), IDCPL(100), PHD(20)
                 LAMSYS (100)
              IENTR, IEXIT, FOD, NUT, NUT, NUT, NUT3, NUT4, NUT5, NUT6, NUT7, NUT8
                   NUT9;NUT10,NUTI1,NUT12
      COMMON /NLINEZ/ PUHY1 /LSTART/ DUMY2(30)
       COMMON /MORKVC/ LNGTHW/W(200)
       FQUIVALENCE (SS(1),S(1,1)),(SS(1),S12(1,1)),(SS(1),S21(1,1))
                 (A(1,1), GAMA(1,1))
                 (SS(10001),PHY(1,1))
       DATA KD1,KD2,KD3,KD4;KD5,KD6,KD7,KD8/100;200;2,20,300,21,6,100/
       DATA LL1, LL2, LL3, LL4, LL5, LL6, LL7, LL9, LL10, LL11, LL12/11*1060/
       DATA PHD(1)/120HPHY1 PHY2 PHY3 PHY4 PHY5 PHY6
                                                              PHY7 PHY8
          PHY10 PHY11 PHY12 PHY13 PHY14 PHY15 PHY16 PHY17 PHY18 PHY19 PH
 $Y20 /
1000 FORMAT (1615)
 2003 FORMAT (///10X'ENTRY POINT'15,4X'HAS BEEN COMPLETED, 1)
 2008 FORMAT (///10x IENTRY = 115,10x NBKSB = 115)
      REWIND HUT9
       LL9 = 1
       BEMIND HOLS
             (YUT8) MSUBT, NNDOF, NCPLT, IDCPL, KCPL, IDPHY, KEEP, KSK
       READ
                   KSR, N, M, M1, M2, M1P1, NSYM, MSYM
                   IENTRY = 6
 9006
  BACKSUBSTITUTION
       READ (5,1000) NBKSB
       CALL PAGEHD
      WRITE (6,2003) IENTRY, NBKSB
      CALL RIAPDS (LAMSYS, NR, NG, ANM, 1,5, LL3, NUT3)
      DO 490 JU=1 NBKSB
      CALL BAKSUB (GAMAIS12,521,53,5,LAMSYS,ID,TV,DV,T1,T2,T3,N,M,NMI
                   KD5, KD1, KD2, 6, LL3, NUT3, 2, LL3, NUT3, 1, LL3, NUT3)
      CALL MTAPDS (T2,1,NMD,6HLAMAKS,1,LL9,LL9,NUT9)
      CALL PHYSCL (PHY,S.A,GAMA, NADOF, KEEP, KSK, KSR, IDPHY, N, 1, MMD
                   KD17KD5,KD4,KD3,KD6,LL9,LL97NUT970,0,0,LL6,NUT6,PHD)
 49 ը
     CONTINUE
      CALL EOF 3 (LL9, NUT9, 0, 0, 0, 0)
 9990 CALL PAGEND
      WRITE (6,2003) TIENTRY
      END
WORDS OF MEMORY TUSED BY THIS COMPILATION
```

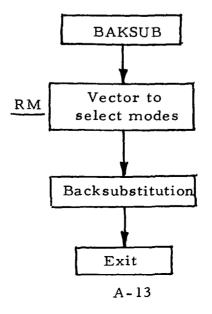




A-11







APPENDIX B

SUBROUTINE EXPLANATIONS

This appendix contains a brief description of the subroutines specifically generated for DAMUS. Some of the subroutines may be used in a general FORMA program. The following list of general subroutines were used by DAMUS. Detailed explanations of each routine are contained in the subroutine comment cards.

Subroutine Names

ALPHAA	LTAPE	START
BTABA	MULTZ	SYMLH
BTABZ	NEGATS	TRANS
BTAZ	NEWMOD	WRITE
BTB	ORDER	WRITIM
COLMLT	PAGEHD	WTAPE
COPY	PRINT	ZERO
DCOM1	PRINTI	ZZBOMB
DIAG	READ	
EIGNl	READIM	
INTAPE	REVSYM	
INV4	RTAPE	

Subroutines for DAMUS

ADDLAM	Adds substructure eigenvalues to diagonal elements of single-subscripted, symmetrically stored matrix.
ASMBLl	Assembles K ₁₁ , K ₂₂ partitions in symmetric form.
ASMBL2	Assembles K ₁₂ partition, double subscripts
ASSEM1	Adds K _{CPL} contributions into correct locations of K ₁₁ , K ₂₂ .
ASSEM2	Adds K _{CPL} contributions into correct locations of K ₁₂
BAKSUB	Backsubstitutes eigenvectors
BSOLVS	Solution for Z of equation $[A][Z] = [B]$ where $[A]$ is symmetrically stored.
BTABSA	Matrix triple product Z = B A B where A is symmetrically stored. Z is double-subscripted but only upper-half is returned.
CNNCTV	Calculate connectivity for substructures.
CPLSPG	Generates spring contributions of 2 substructures in partitioned form.
DCMSYM	Decomposes symmetrically stored matrix A into factors where A = $L D L^T$
DELCPL	Changes data files when changing a coupling spring
DE LPHY	Changes data files when changing physical vectors to be printed
DE LSUB	Changes data files when changing basic substructure data
EIGVEC	Gets eigenvalues and complete set of participation factors
EOF3	Write end of file for up to 3 files at a time
GETPHY	Used to generate substructure vector matrix for obtaining physicals

IDFILL	Special routine which fills up vector for omitted values
INDCES	Generates initial data and index locations
KEEPV	Generates vectors for assembling K matrix
KSTAR	Generates reduced stiffness matrix
MODE 2	Eigenvalue/vector routine with mass matrix options
MSTAR	Generates reduced mass matrix
MULTBS	Multiplies BZ = A * BZ where A is symmetrically stored
NEWPHY	Generates new set of eigenvectors in partitioned form for getting physicals
PHYSCL	Calculates physical eigenvectors
REVAZZ	Revises matrix A into matrix Z, where Z may be a single or double subscripted matrix
RMAT	Calculates [R] for dynamic transformation
ROTATA	Special triple product $Z = R^T$ A R when a 3X3 submatrix of direction cosines is input for R.
RTAPDS	Special matrix read tape routine - double subscript
RTAPSS	Special matrix read tape routine - single subscript
SUBDAT	Generates substructure eigenvalues and vectors from basic substructure mass and stiffness matrices
TRANSA	$B = A^{T}$ where A, B occupy the same core location
UNPAKS	Unpacks symmetric single-subscripted array into symmetric double subscripted storage (upper half only)
UPDFIL	Updates data from two files to one in a predescribed order
UPDPHY	Updates data file for physical vectors
WTAPDS	Special matrix write tape routine - double subscripts
WTAPSS	Special matrix write tape routine - single subscripts

APPENDIX C

SAMPLE PROBLEM

This appendix contains a sample problem using all 6 entry points of DAMUS.

The sample problem used to illustrate the use of DAMUS was

Problem 1, a 20 DOF longitudinal rod model consisting of 2 substructures

(10 DOF/substructure). The output data printed by DAMUS follows a

listing of the actual data cards used to execute the program.

Since this was only a test case, no output tapes were saved and the same logical tape unit was assigned to the input files 7, 8 and 9.

Normal execution of DAMUS would require different logical unit numbers.

INPUT DATA CARDS

```
E.J. KUHAR
STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1
20 DOF LONGITUDINAL ROD
                                 2 SUBSTRUCTURES
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               12
                     13
                           14
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l į	ONEGA (RAD/SEC)	(4)	(.5)		(.7)	(8)	(6)	. (20)
:	117, 0176E_002, 0880E01 3,4228E .01	426734E 01	5,8088E 01	6,8013E 01	7.6262E.01	8.2634E 01	. 8.6971E .01.	α)
i	FREQ (HZ) (3)	(4)	(5)	(9)	(7)	(8)	(6)	(10)
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RUN NO. STCA01		RUN B	E 053173				PAGE .NO	មា
STIFFNESS COUPLING CHECK C 20 DOF LONGITUDINAL ROD	CASE FROM ENTRY	RY ROINT 1 TURES						;
(10 x 10) (2)	(3)	. (4)	(5)	(9)	(7)	(8)	(6)	(16)
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RUN NO, SICAO1	PAGE NO.
STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1 20 DOF LONGITUDINAL ROD 2 SUBSTRUCTURES.	
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RUN NO, SICADI STIFFNESS COUPLING CHECK CASE FROM ENTRY ROINT 20 DOF LONGITUDINAL ROD	SUBSTRUCTURE E ORDER	1 1 1 2 3 4 5	C-13

STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1 1 1 1 1 1 1 1 1 1	STIFFNESS COUPI									
(5) (6) (7) (8) (9) (10) 03 2:7639E 03 4:0000E 03 5.2361E 03 7:2361E 03 7:2861E (5) (6) (7) (8) (-9) (10) 01 5:2573E 01 6:3246E 01 7.2361E 01 7:9694E 01 8:5065E 01 8:8342E (5) (6) (7) (8) (9) (10) 00 8:3673E 00 1:0066E 01 1.1517E 01 1.2684E 01 1:3539E 01 1:4060E	20 DOF LOUGITUI	LING CHECK CA	SE FROM ENTR	TURES						
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	STIFFNESS CC 20 DOF LONGI	STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1	ASE FROM EN	TRY POINT 1							
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_	10 X 10)	(2)	(3)	(4)	(2)	(9)	(7)	(8)	(6)	(116)	
=	1 3,1623E=0	4	4,2533E=01	+1	3,5180E-01	3.1623E=01	2.6287E=01		1.3820E-01	6:9960E-02	
	1.3,1623E=01	n	2,6287E=01	\sim	-1,3620E-01	-3,1623E=01	-4.2533E-01.	64,4171E=01.		-2:0303E-01	;
~	1 3,16236=01	<u>بر</u>	-2,1053E-08	=3:1623E-01	c4,4721E-01	-3,1623E=01	-1.296nE=08	3,1623E=01	4,4721E-01	3:1623E-01	
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6	1.3,1623E=0	4	-4,2533E=01	<u>۔</u> س	3,6130E-01	-3.1623E=01	-2.6287E=01.	ا. آ	1.3820E=01	-4:4171E-01	
^	1 3,16235=0	1 22	-2,6287E-01	4,4171E-01	=1,3820E-01	-3,1623E-01	4,2533E=01	, ii	-3.6180E-01	3,9847E-01	
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STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1 20 DOF LONGITUDINAL ROD 2 SUBSTRUCTURES		
CARD INPUT INTEGER MATRIX IPDOF (1 X 3)	SELECTS DOF TO BE PRINTED	0
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RUN BY E.J. KUHAR	ROM ENTRY POINT 1	SUBSIRUCTURE 2 HAS 10 DOF WITH 1 ROUNDARY DOF DEFINED.	(6) (7) (8) (9) (10) (11) (12) (13) (14) (15) (16) (17) (18) (19) (20)	6 7 8 9 10			
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STIFFNESS COUPLING CHECK CASE FROM ENTRY ROINT 1 20 DOF LONGITUDINAL ROD 2 SUBSTRUCTURES	
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PAGE NO. 15					
DATE 053173 RUN BY E.J. KUHAR CHECK CASE FROM ENTRY POINT 1 ROD 2 SUBSTRUCTURES	= 1 10P = 0				
RUN NO, SICAO1 STIFFNESS COUPLING CHECK CASE 20 DOF LONGITUDINAL ROD	IENIRY = 2 NCPLS.=		C-19		

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STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1 20 DOF LONGITUDINAL ROD 2 SUBSTRUCTURES	
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RUN NO. STCA01. PAGE NO. 18 F.J. KUHAR
STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1 20 DOF LONGITUDINAL ROD. 2 SUBSTRUCTURES
I ENTRY = 3
CARD INPUT INTEGER MATRIX KEEP (2 X 2) SELECTS KEPT/REDUCED DOF'S
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RUN-NO, SICA01	DATE 053173 RUN BY E, J. KUHAR	PAGE-NO, 19
STIFFNESS COUPLING CHECK CASE FROM ENTRY ROINT 20 DOF LANGITUDINAL ROD 2 SUBSTRUCTURES	1 L2 I	
LENTRY = 4		
CARD INPUT MATRIX LAMDAO (1 X 1)	P.+2 REDUCTION FREQUENCY	0
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		(7)		(2)		(7)			
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DATE 053173 RUN BY E.J. KUHAR		(2)		(5)		(6)			
	TRY ROINT 1	(4)	6.5858E 02	(4)	2,5663E 01	(4)	4.0844E 00	:	
: ; ;	ASE FROM ENT 2 SUBSTRUC	(3)	3,0615E 02	(.3)	1;7497E 0Î	(3)	2,7848E 00		
	LING CHECK C	(2)	1,1057E 02	(1.2)	1,0515E.01.	(2)	1,6736E 00		
-STCA01	STIFFNESS COUPLING CHECK CASE FROM ENTR	(4)	1 1,2331F 01 1,1057E 02 3,0615E 02	OMEGA (RAD/SFC) (.3)		FRED (HZ)	1 5,5887E=01 1,6736E 00 2,7848E 00		
RUN -NOSTCA01		LAMSYS (1)	-	OMEC		F.REG	1		 C-2

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STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1	
1ENTRY = 5 MD1 = 1	
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STIFFNESS COUPLING CHECK CASE			RUN BY	UN BY E.J. KUHAR	IAR				
~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	ING CHECK C	ASE FROM ENTRY POINT	V POINT 1						
(10 x 4)	(2)	(3)	(4)	(2)	(9)	(7)	(8)	(6)	(16)
		7831F=01	2.9803E=01 3.9466E=01	de designation de la constitució	de die nach de marche de le prime de l'improduction ou				
3 1 1 7570E=01 3	3,0988E-01	5,8406Ea02	3.3656E=01			American de la companya de la compan	****		
1 1,32426=01	3.0359E-01	6207E=01		 - - -					
1 8,58266602	2,3264E-01	1423501	3.1519E=01						
	1,7656E+01 1,1021E-01	./352E=01 :							
	3,7472E-02	4967E=02.	8.9395E						
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STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1						
0 X 4) (2)	(5)	(9)	ر می	(8)	(6)	(10)
3230E=01 1,9335E+01 =2,8130E=01						
Additional 1. Subsetul as . 2550E au						
6.1967E-02						
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3 0431File 10 1444File 2 1600Files						
1016E01.=2.6338E-011.7367E01						
1409E=01 =2,9875E=01 2,4941E=01						
1607Emol_m3,1706E*012,8976Em01						
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STIFFNESS COUPLING CHECK CASE FROM ENT 20 DOF LONGITUULNAL ROD 2. SUBSTRUC	
IENIRY = 6 NBKSB = 1	
CARD INPUT INTEGER MATRIX IMODE (1 X 4) SELECTS MODES FOR BACKSUBSTITUTION	0
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MODES SELEGIE	ED_FOR_BACKSUE	MODES SELECTED FOR BACKSUBSTITUTION (1 X 4) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11)	(12)	(13) (14)	(45)	(16) (17)	(18)	(19) (50)	1	:
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STIFFNESS COUPLING CHECK CASE FROM ENTRY POINT 1 20 DOE LONGILUDINAL ROD 2 SUBSTRUCTURES	and the second of the second o				
RATIO (LAM2/LAM1) (2) (3) (4)	(5) (6)	(7)	(8)	(6)	(18)
1 1 1:000nE 00 9,9954E-01 9,9470E=01 9.0210E=01				فاستعدن بدريت بإن فرينسيد ومنسي كانت يوازيند	
FNORM FROM MASS NORMALIZATION (3) (4)	(5) (6)	(7)	(8)		(10)
(1 X 4) (2) (3) (4)	(5) (6)	(7)	(8)	(6)	(10)
1 1 1,233JE 01 1,1052E 02 3,0453E 02 5,941JE 02					£
OMEGA (RAD/SEC) (1 X 4.) (2) (.3)	(-5)	(7)	(8.)	(6)	(16)
1. 3.5115E.00 1.0513E 01 1.7451E 01 2.4374E 01	#				
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1 1 5,5887E=01 1,6732E 00 2,7774E 00 3.8793E 00					
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DATE 053173		(5)											
RUN B	RY POINT 1 TURES	(4)	2.6118E=01	2.3735E=01	5755E 5011E	3728E	=1.8997E=01			-			the saled of the first state of the sales and the sales and the sales and the sales are sales and the sales and the sales are sales and the sales are sales
	ASE FROM ENTRY POINT 2. SUBSTRUCTURES	(3)	7859E	5.8669E=02	5455E=01	1534E=01	7943E=01	į					
	ING CHECK C/	(2)	2.4825E-01	3,0994E-01	3.0422E-01 2.7583E-01	2,3219E-01	1,0947E-01	-	-				
	STIFFNESS COUPLING CHECK CASE 20 DOF LONGITUDINAL ROD	4)	100	7569E=01	3239E=01	202	7169E=02						
-RUN-NO -SICA 01	ST11 20	PHY1	100	₩ 4	5 1	9	10 1		relimente de debito de destro de contra de con		C-	31	

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Space Division	☐ Evendale, Ohio	Huntsville, Ala.	☐ Bay St. Louis, Miss.	☐ Houston, Texas
· /	Sunnyvale, Calif.	☐ Roslyn, Va. ☐ Bel	ltsville, Md.	